

# High Pressure Sintering of Al<sub>2</sub>O<sub>3</sub>-CNT Nanocomposites

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## Article Information

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Alumina is one of the most widely used ceramic materials owing to its relatively high hardness (15-22 GPa), good oxidation resistance and chemical stability with iron or steel [1]. However applications have been limited due to its low fracture toughness. In most cases, low addition of carbon nanotubes as reinforcement improves the fracture toughness, on the other hand it degrades the hardness or strength. Carbon nanotubes (CNTs) have recently been considered as reinforcing elements in ceramic matrix composites due to their unique mechanical properties [2-4].

Carbon nanotubes tend to be agglomerated each other owing to a strong van der Waals attractive force. There have been several attempts to fabricate carbon nanotube reinforced ceramic matrix nanocomposites. To create functional CNT-reinforced composites, two main problems have to be overcome:

1. Homogeneous dispersion of nanotubes in the matrix
2. Generation of strong interfacial bonding between CNTs and the matrix [1, 5-7].

Dense and nanostructure alumina ceramics are widely used in practical applications due to its outstanding mechanical, electrical and optical properties. It is difficult to

In this study, Al<sub>2</sub>O<sub>3</sub>-CNT nanocomposites were sintered at 800-1000 °C under 5 GPa for 10 minutes using two different powders as starting material,  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> and AlOOH. The effect of transition alumina powders on the properties of the high pressure sintered Al<sub>2</sub>O<sub>3</sub>-CNT nanocomposites were studied. Al<sub>2</sub>O<sub>3</sub> ceramics have been widely used for structural, electrical and optical applications. Carbon nanotubes (CNTs) have recently been considered as reinforcing elements in ceramic matrix composites due to their unique mechanical properties. Reactive pressure sintering at low temperatures took place during the fabrication of CNT reinforced ceramic composites to avoid the agglomeration of carbon nanotubes. The hardness and densities were investigated and correlated with the microstructure of the dense materials. SEM analysis was used to determine the CNT distribution in the matrix, the morphology and size of the particles.

obtain a fully dense ceramic with nanocrystalline grain size. The transition paths and temperatures vary depending on the particle size, chemical homogeneity, heating rate, and water vapor pressure [8, 9].

However attempts by applying high sintering pressure proved useful in achieving higher densities with nanocrystalline microstructure [10]. Transition alumina powders normally have the highest surface area and smallest crystalline size, e.g. 15-70 nm [11].

The objective of this study was to investigate the effect of transition alumina powders on the properties of the high pressure sintered Al<sub>2</sub>O<sub>3</sub>-CNT nanocomposites.

## Experimental Procedure

Two different alumina ( $\gamma$ -Al<sub>2</sub>O<sub>3</sub> and AlOOH) powder were used as starting materials in this study. The first starting powder consists of spherical  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> (JSPDS Card No: 00-046-1215) phase with an average particle size of 20 nm (Plasma & Ceramic Technologies Ltd.-Latvia) and specific surface area of 50 m<sup>2</sup>/g in the granulated state. The chemical composition of the starting  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> powder was given in Table 1. The second material used as a starting material for Al<sub>2</sub>O<sub>3</sub>-CNT com-

posites is AlOOH obtained by hydrothermal processing.

**Preparation of CNT reinforced  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> powder.** A suspension of  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> powders were prepared. Ethanol is used as a solvent and the weight percentage of alumina in the suspension was 5%. A suspension of CNT (20 nm in diameter and 10-25  $\mu$ m in length), (Thomas Swan Co. Ltd., UK), was also prepared in ethanol in the weight percent of 1%. Both suspensions were ball milled and ultrasonicated for 2 hours. The CNT suspension was added to the alumina suspension dropwisely. Then the composite powders were obtained after the drying process.

**Preparation of CNT reinforced AlOOH (boehmite) powder.** Aluminum acetate powders (2Al(OH)(C<sub>2</sub>H<sub>3</sub>O<sub>2</sub>)<sub>2</sub>) and CNT were mixed. The mixture was stirred in distilled water. 17 ml 25% ammonia solution (NH<sub>3</sub>) was then added to the mixture to adjust the

Chemical impurities [ppm]	Fe	Si	Na
According to supplier's analytical certificate	<1000	<200	< 1000

Table 1. Chemical impurities of the starting  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> powder

pH above 9 in order to obtain fine boehmite particles. The reason for the addition of such quantity of CNT in the mixture was the aim of obtaining 1% reinforced final structure which was going to be in the form of CNT reinforced alumina ( $\text{Al}_2\text{O}_3$ ) after the heat treatment. The resultant mixture was transferred into a teflon lined autoclave approximately filling 80% of the 500 ml total volume and the hydrothermal synthesis was performed at 200 °C for 2 hours in a high pressure autoclave. The pressure of the autoclave was approximately 1 MPa. The autoclave was then cooled to room temperature. The resultant solution was vacuum filtered for four times to remove water soluble impurities. Then, the filtered solution was dried in an autoclave at 110 °C. Finally, CNT reinforced boehmite powder was obtained.

**Sintering Conditions of  $\text{Al}_2\text{O}_3$ -CNT Nanocomposites.**  $\gamma\text{-Al}_2\text{O}_3$  or  $\text{AlOOH}$ -CNT powder containing no additives was uniaxially

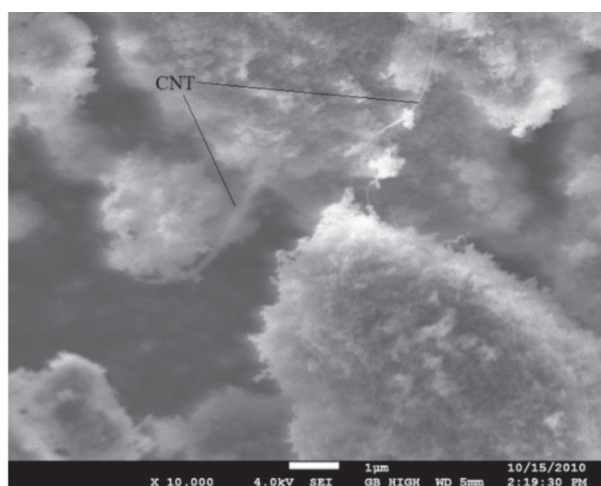
cold pressed at 20 MPa into cylinders 20 mm in diameter and 10mm in height. All the green compacts were pellets of 4 g. Green compact was encapsulated in a cube die made of pyrophyllite. The  $\text{CNT-Al}_2\text{O}_3$  bodies were fabricated in cubic anvil high pressure (5 GPa) and at a temperature of 800 °C for 10 minutes. Phase analysis of the sintered samples was carried out by X-ray diffraction (XRD). Grain sizes were estimated from high-resolution scanning electron micrographs taken from fracture surfaces. Microhardness was determined on the polished surfaces under the load of 500 g.

## Result and Discussion

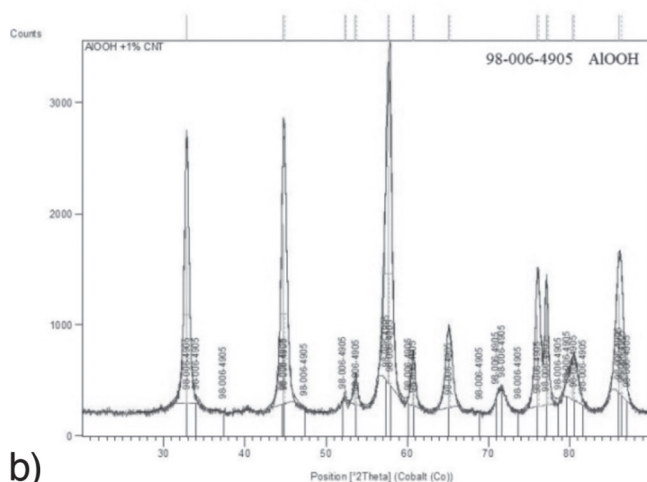
The SEM micrograph and the XRD spectrum of the  $\text{AlOOH}$ -CNT composite powder obtained by hydrothermal processing are presented in Figure 1. As can be seen in the figure,  $\text{AlOOH}$  and CNT are obtained.

The SEM micrograph and the XRD spectrum of  $\text{Al}_2\text{O}_3$ -CNT nanocomposites ( $\gamma\text{-Al}_2\text{O}_3$  used as starting material) sintered at 800 °C under 5 GPa for 10 minutes are presented in Figure 2.  $\gamma\text{-Al}_2\text{O}_3$  transformed to  $\alpha\text{-Al}_2\text{O}_3$  in this sintering conditions (Figure 2b). After sintering, average grain size of  $\alpha\text{-Al}_2\text{O}_3$ -CNT is 150 nm and agglomeration of CNT in the microstructure can be seen in Figure 2a. An alumina hydrate,  $\text{AlOOH}$ , was found in the samples sintered at 5 GPa and 800 °C as can be seen in Figure 2b. This phase is caused by trapped water or surface OH groups which forms the hydrate phase during low temperature sintering.

The SEM micrograph and the XRD spectrum of  $\text{Al}_2\text{O}_3$ -CNT nanocomposites ( $\text{AlOOH}$  used as starting material) sintered at 800 °C under 5 GPa for 10 minutes are presented in Figure 3. The average grain size of  $\text{AlOOH}$ -CNT composite is 3  $\mu\text{m}$ . Accord-

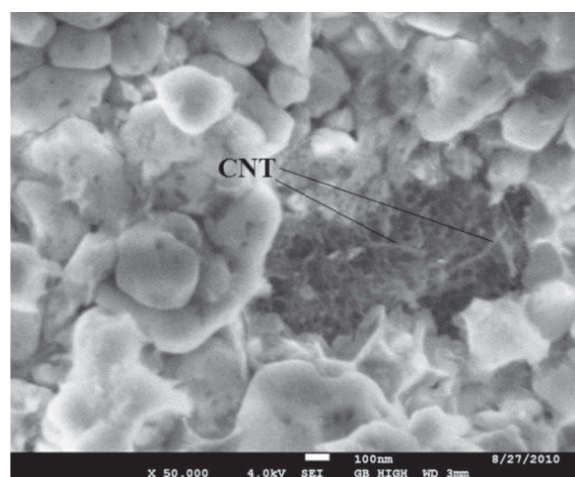


a)

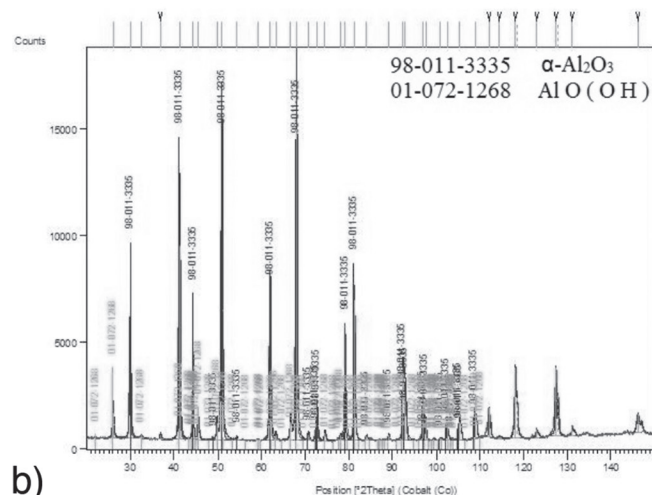


b)

Figure 1.  $\text{AlOOH}$ -CNT composite powder obtained by hydrothermal processing, a) SEM micrograph, b) XRD spectrum

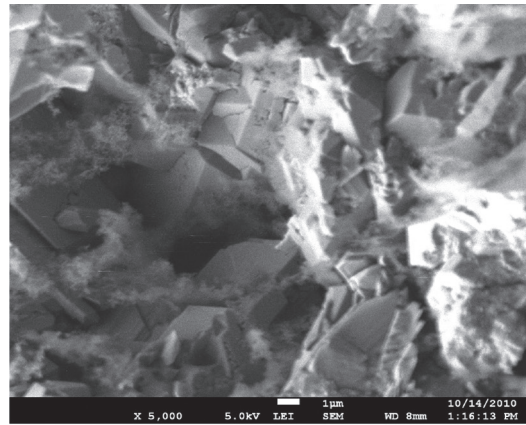
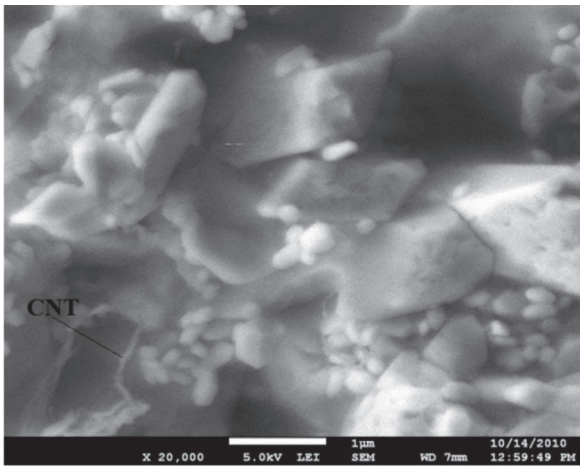


a)

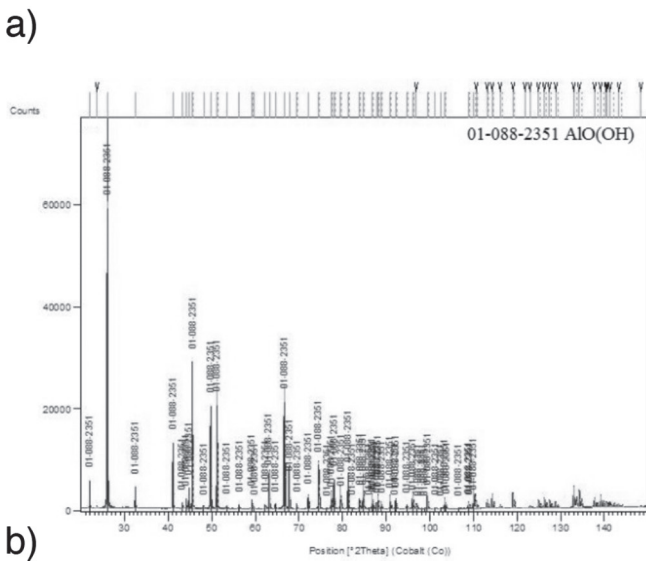


b)

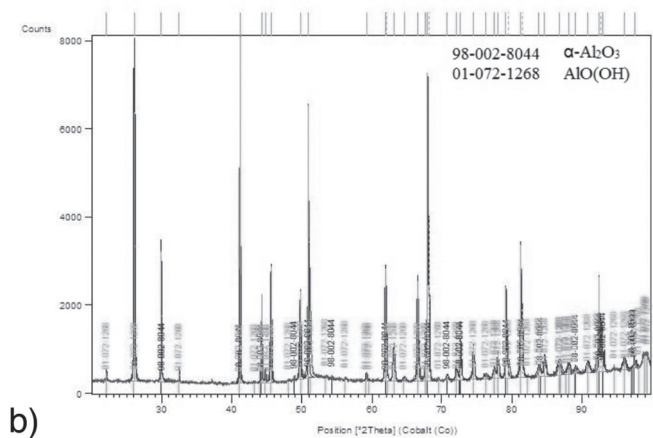
Figure 2.  $\text{Al}_2\text{O}_3$ -CNT nanocomposite ( $\gamma\text{-Al}_2\text{O}_3$  used as starting material) sintered at 800 °C under 5 GPa for 10 minutes, a) SEM micrograph, b) XRD spectrum



a)



b)



b)

Figure 4.  $\text{Al}_2\text{O}_3$ -CNT nanocomposite (AIOOH used as starting material) sintered at  $1000^\circ\text{C}$  under 5 GPa for 10 minutes, a) SEM micrograph, b) XRD spectrum

Figure 3.  $\text{Al}_2\text{O}_3$ -CNT nanocomposite (AIOOH used as starting material) sintered at  $800^\circ\text{C}$  under 5 GPa for 10 minutes, a) SEM micrograph, b) XRD spectrum

ing to XRD spectrum, phase transformation did not occur.

The SEM micrograph and the XRD spectrum of  $\text{Al}_2\text{O}_3$ -CNT nanocomposites (AIOOH used as starting material) sintered at  $1000^\circ\text{C}$  under 5 GPa for 10 minutes are presented in Figure 4. Average grain size of  $\alpha$ - $\text{Al}_2\text{O}_3$ -CNT composite is  $5\ \mu\text{m}$ . According to XRD spectrum, phase transformation occurred, the presence of the  $\alpha$ - $\text{Al}_2\text{O}_3$  could be seen. In the presence of the hydrates, it is difficult to control grain growth according to S. C. Liao et al. [10].

Sintering  $\gamma$ - $\text{Al}_2\text{O}_3$ -CNT at 5 GPa/ $800^\circ\text{C}$  for 10 minutes resulted in compacts with a theoretical density of 95.40% and with a hardness of  $882.62\ \text{kg} \times \text{mm}^{-2}$ .

Sintering AIOOH-CNT at 5 GPa/ $800^\circ\text{C}$  for 10 minutes resulted in compacts with a theoretical density of 84.34% and with a hardness of  $472.95\ \text{kg} \times \text{mm}^{-2}$ .

## Conclusions

- Dense and crack free compacts were obtained by high pressure processing at 5 GPa/ $800$ - $1000^\circ\text{C}$  for 10 minutes.
- CNT agglomerated in  $\gamma$ - $\text{Al}_2\text{O}_3$  powder prepared with ethanol, whereas CNT was dispersed homogenously in AIOOH prepared by hydrothermal processing.
- The theoretical density of  $\gamma$ - $\text{Al}_2\text{O}_3$ -CNT nanocomposite sintered at 5 GPa/ $800^\circ\text{C}$  for 10 minutes is 95.40%, while the theoretical density of AIOOH-CNT composite sintered at the same conditions is 84.34%.
- An average grain size of 150 nm is obtained in the  $\gamma$ - $\text{Al}_2\text{O}_3$ -CNT nanocomposite sintered at 5 GPa/ $800^\circ\text{C}$  for 10 minutes. But in the AIOOH-CNT composite sintered in the same conditions, the average grain size is 3  $\mu\text{m}$ .

- The microhardness of  $\gamma$ - $\text{Al}_2\text{O}_3$ -CNT nanocomposite is almost the two times the value of microhardness of AIOOH-CNT composite. The reason for this is the difficulty of the control of grain growth due to the presence of the hydrates.

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## Abstract

**Hochdrucksintern von Al<sub>2</sub>O<sub>3</sub>-CNT Nanokompositen.** In der diesem Beitrag zugrunde liegenden Studie wurden Al<sub>2</sub>O<sub>3</sub>-CNT Nanokomposite bei 800 bis 1000 °C unter 5 GPa für 10 Minuten unter Verwendung von zwei verschiedenen Pulvern  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> and AlOOH gesintert. Die Auswirkung der Übergangsaluminiumpulver auf die Eigenschaften der Hochdruck-gesinterten Al<sub>2</sub>O<sub>3</sub>-CNT Nanokomposite wurde untersucht. Al<sub>2</sub>O<sub>3</sub> Keramiken werden breitflächig für strukturelle, elektrische und optische Anwendungen eingesetzt. Carbon-Nanoröhrchen (Carbon Nanotubes (CNTs)) finden in der letzten Zeit als Verstärkungselemente in Keramikmatrixkompositen aufgrund ihrer einzigartigen mechanischen Eigenschaften Berücksichtigung. Während der Fertigung der CNT-verstärkten Keramikkomposite wurde das Reaktivdrucksintern bei niedrigen Temperaturen angewendet, um die Agglomeration der Carbon-Nanoröhrchen zu vermeiden. Die Härte und die Dichte wurden untersucht und mit der Mikrostruktur der dichten Materialien korreliert. Eine REM-Analyse wurde durchgeführt, um die CNT-Verteilung in der Matrix sowie die Morphologie und die Größe der Partikel zu untersuchen.

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